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# TOWARDS ZERO EMISSION ROAD CONSTRUCTION – THE USE OF RECYCLED MATERIALS IN PAVEMENT STRUCTURES

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#### **Background**

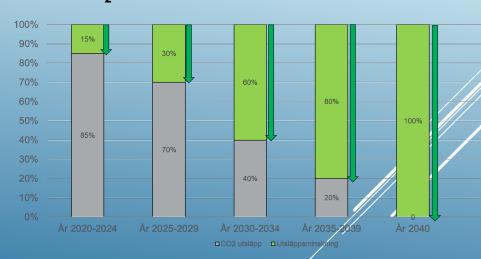
The Swedish Transport Administration (Trafikverket (TRV)) has set the goal of achieving climate neutral infrastructure by 2040.

To reach this goal, increased usage of residual and recycled materials in road constructions is indispensable.

Construction and industrial waste (CIW) materials from various industries are mostly piled up and dumped as landfill.

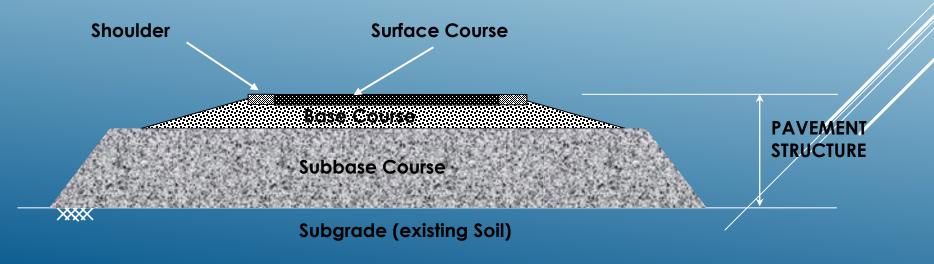
Replacing the fresh aggregates with recycled or residual materials has the potential of significant positive impact towards circular economy and climate neutrality.

#### CO<sub>2</sub> reduction



# Objective

To investigate several recycled and residual (CIW) materials for their potential usage in pavement structures and to create the necessary design basis for this, particularly by updating the ME design tool ERAPave PP.



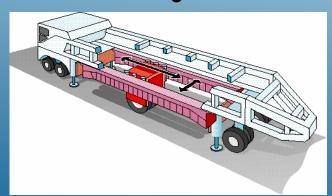
# The approach - Divided into three main steps:

- 1. Small-scale Multi-Stage (MS) Repeated Load Triaxial (RLT) laboratory testing.
- 2. Full-scale Accelerated Pavement Test (APT) using a Heavy Vehicle Simulator (HVS).
- 3. In-service pavement monitoring.

#### Small-scale MS RLT testing



**Full-scale APT using HVS** 

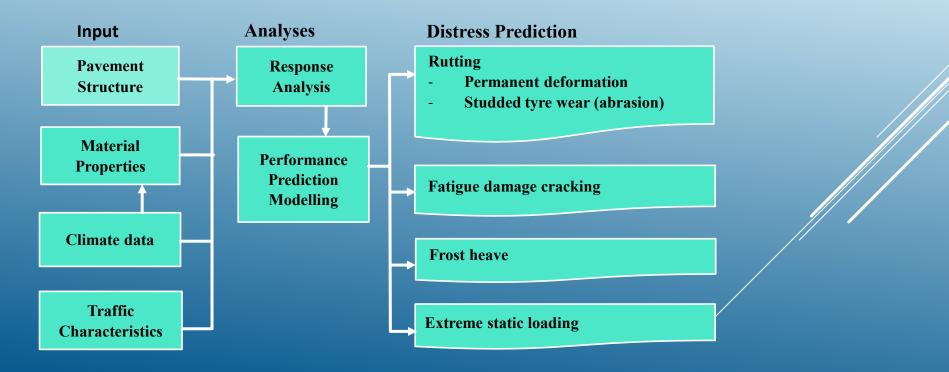


In-service road



### **ERAPave PP** (Elastic Response Analysis of Pavements – Performance Predictions)

A new M-E pavement design method has been developed in Sweden.

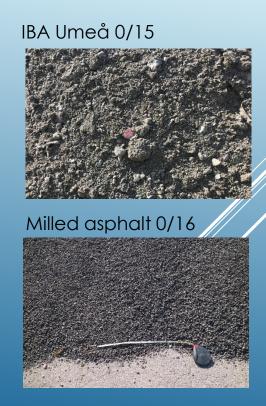


## Four CIW materials were tested in this project:

Incinerated Bottom Ashes - IBA
Umeå 0/15
Sysav 0/45
Crushed concrete 0/64
Milled asphalt 0/16

Crushed concrete 0/64

IBA Sysav 0/45



### The four materials



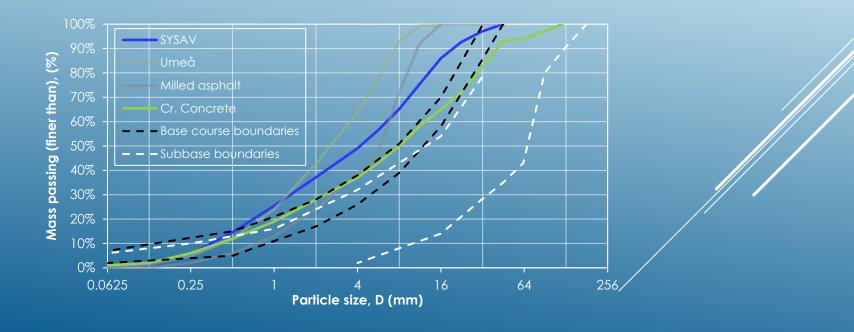






#### Grain size distribution curves

The grain size distribution curve does not fulfil boundaries of base course or subbase materials.



## The laboratory testing

Multi-Stage Repeated Load Triaxial (**MS RLT**) testing was done to investigate the performance properties of the waste materials.

- Cylindrical specimens (d = 150 mm, H = 300 mm).
- Vibrocompaction, free drainage conditions.
- Constant confining pressure (air) with cyclic axial loading (10 Hz) with no rest period (Haversine pulses).

Resilient properties -  $M_R$ Permanent deformation properties - PD30 stress paths, 10,000 load repetitions.

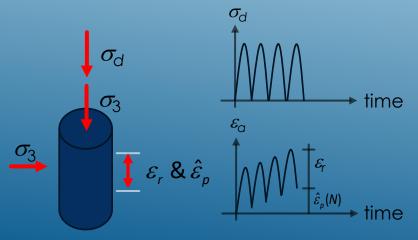
# Stress paths (low stress levels) Resilient $(M_r)$ & Permanent Deformation (PD) properties

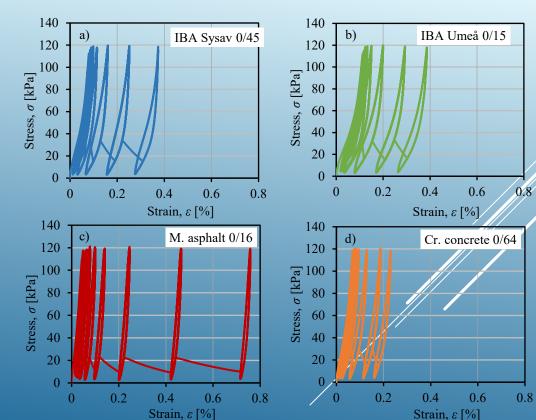
30 stress paths, 10,000 load repetitions.

			Low stress level													
	Sequence 1			Sequence 2			Sequence 3			Sequence 4			Sequence 5			
	Confining stress, σ <sub>3</sub> kPa	Deviator stress, σ <sub>d</sub> kPa		Confining stress, σ <sub>3</sub> kPa			Confining stress, σ <sub>3</sub> kPa	Deviator stress, $\sigma_d$ kPa		Confining stress, σ <sub>3</sub> kPa	Deviator stress, $\sigma_d$ kPa		Confining stress, σ <sub>3</sub> kPa	Deviator stress, σ <sub>d</sub> kPa		
	constant	min	max	constant	min	max	constant	min	max	constant	min	max	constant	min	max	
1.	20	0	20	45	0	60	70	0	80	100	0	100	150	0	100	
2.	20	0	40	45	0	90	70	0	120	100	0	150	150	0	200	
3.	20	0	60	45	0	120	70	0	160	100	0	200	150	0	300	
4.	20	0	80	45	0	150	70	0	200	100	0	250	150	0	400	
5.	20	0	100	45	0	180	70	0	240	100	0	300	150	0	500	
6.	20	0	120	45	0	210	70	0	280	100	0	350	150	0	600	

# Test results from MS RLT testing

The last stress path in sequence 1 is where  $\sigma_3$  = 20 kPa and  $\sigma_d$  = 120 kPa. The loops correspond to load cycles: 10, 45, 95, 195, 395, 995, 2495 and 4995.





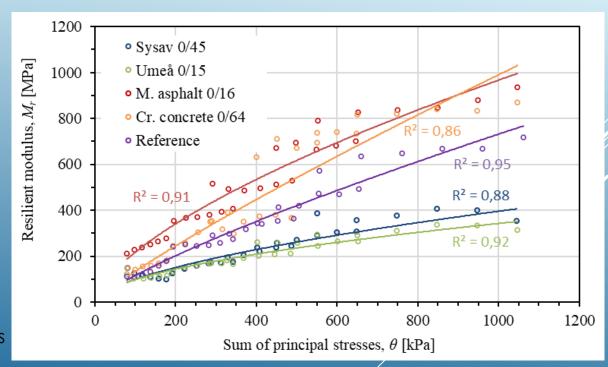
# Resilient properties M,

At 75% of  $W_{opt}$ .

$$M_r = \frac{\sigma_a}{\varepsilon_r}$$

$$M_r = k_1 \left(\frac{\theta}{\rho_a}\right)^k$$

 $k_1, k_2$  Material properties  $\theta$  Sum of principal stresses  $p_a$  Reference stress



## Permanent deformation properties PD

At 75% of  $W_{opt}$ .

Dots – Test results Lines – Modelled results

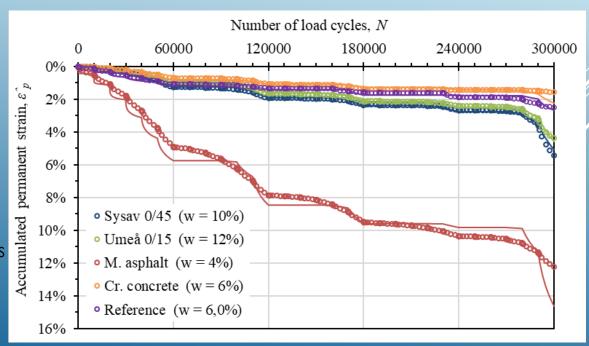
$$\hat{\varepsilon}_{p}(N) = aN^{b(\varepsilon_{r})^{c}} \varepsilon_{r}$$

a, b, c Material properties

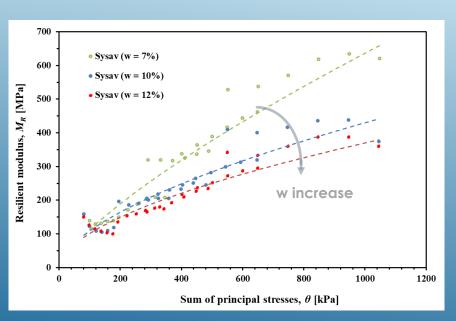
N Number of load repetitions

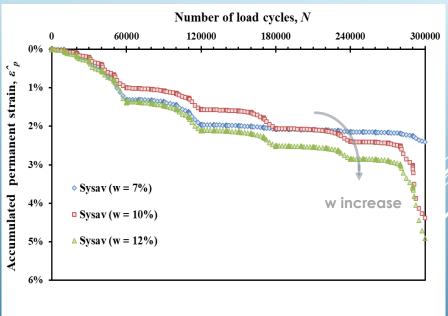
 $\varepsilon_r$  Resilient strain

w Moisture content



## $M_R$ and PD are moisture dependent

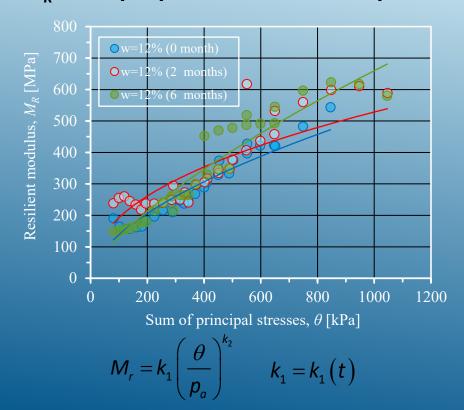


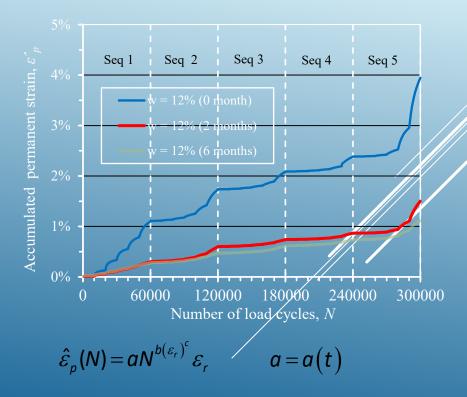


$$M_r = k_1 \left(\frac{\theta}{\rho_1}\right)^{k_2} \qquad k_1 = k_1 (w)$$

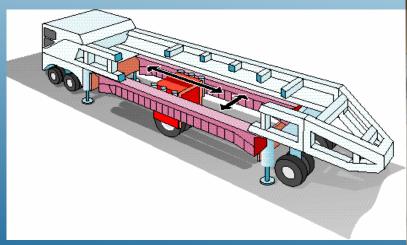
$$\hat{\varepsilon}_{p}(N) = aN^{b(\varepsilon_{r})^{c}} \varepsilon_{r} \qquad a = a(w)$$

# $M_R$ & PD properties are time dependent IBA





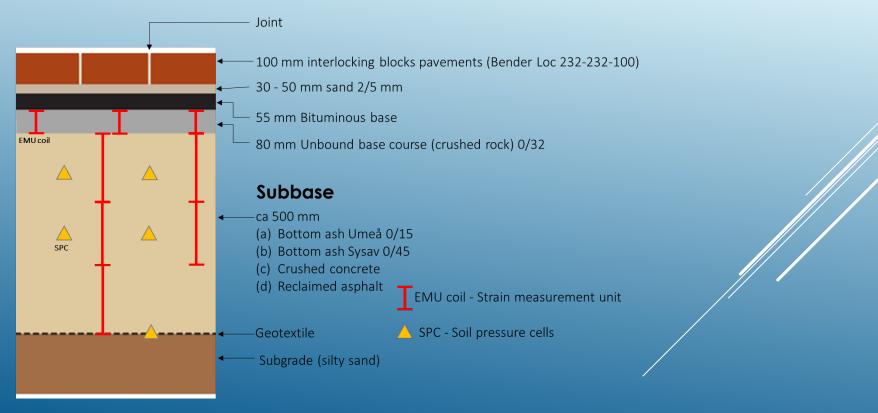
# Full scale APT using an HVS machine





APT = Accelerated Pavement Test HVS = Heavy Vehicle Simulator

#### Four structures were tested.



# **Construction of test objects #1**





# **Construction of test objects #2**



# **Construction of test objects #3 IBA**





# **Construction of test objects #4**





# **Construction of test objects #5**

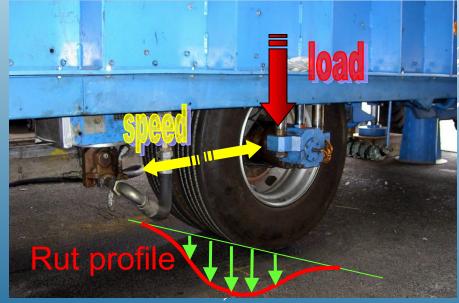




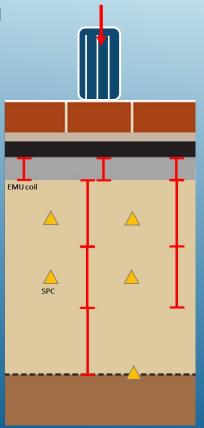
## **Rut development**

HVS was used to measure the rutting development.

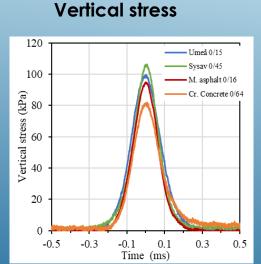
Four testing phases,  $T = 10^{\circ}$ C, speed = 12 km/h. 1st Preloading phase, W = 30 kN, SW, p = 700 kPa 2nd T. Ph. M1 W = 40 kN, DW, p = 800 kPa 3rd T. Ph. M2 W = 60 kN, DW, p = 800 kPa 4th T. Ph. M3 W = 60 kN, DW, p = 800 kPa, raised gwt.

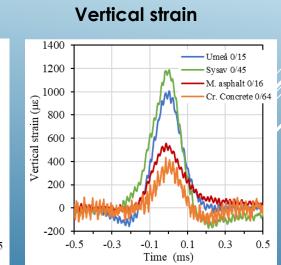


# The HVS testing



### Response from embedded sensors.





# Rut as a function of load repetitions

Surface rut after 400 000 load repetitions
Two incineration bottom ash (IBA) materials as subbase materials.

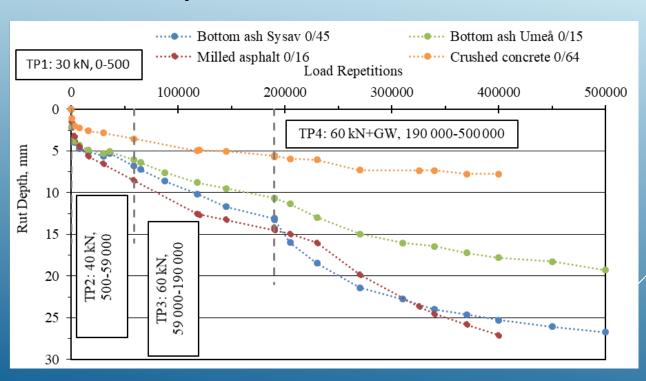


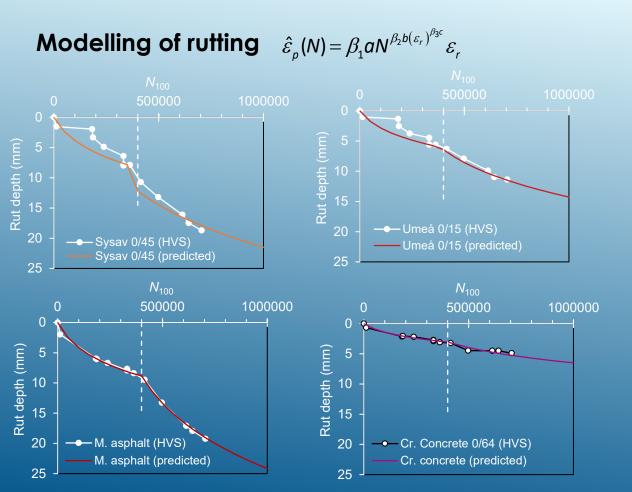


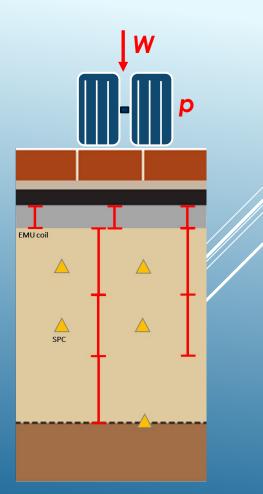
Sysav 0/45 closest and Umeå 0/15 further away

Close-up of the developed rut

## Rut as a function of load repetitions







## **In-service test road**

Regular FWD measurement & rut monitoring





#### **Conclusions**

Construction and Industrial Waste (CIW) materials have been tested to get information about their suitability to be used as unbound subbase materials in pavement structures.

A three step ME approach is used.

- (1) Realistic small-scale MS RLT Lab testing, (2) Full-scale HVS loading (APT) & (3) In-service road monitoring.
- All the CIW materials showed moisture dependent mechanical behaviour (M, and PD).
- They further showed time (age) dependent mechanical behaviour (Increased stiffness and stability with time).
- It was difficult to compact the materials in the full-scale APT. Generally, the achieved degree of compaction was higher in the small-scale RLT lab tests.
- Some calibration of M<sub>r</sub> and accumulation of PD is necessary between small-scale (ab testing and full-scale APT (HVS) testing.
- This discrepancy needs to be eliminated, and some well-established protocol should be developed to deal with it.

# Thank you - questions?

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