



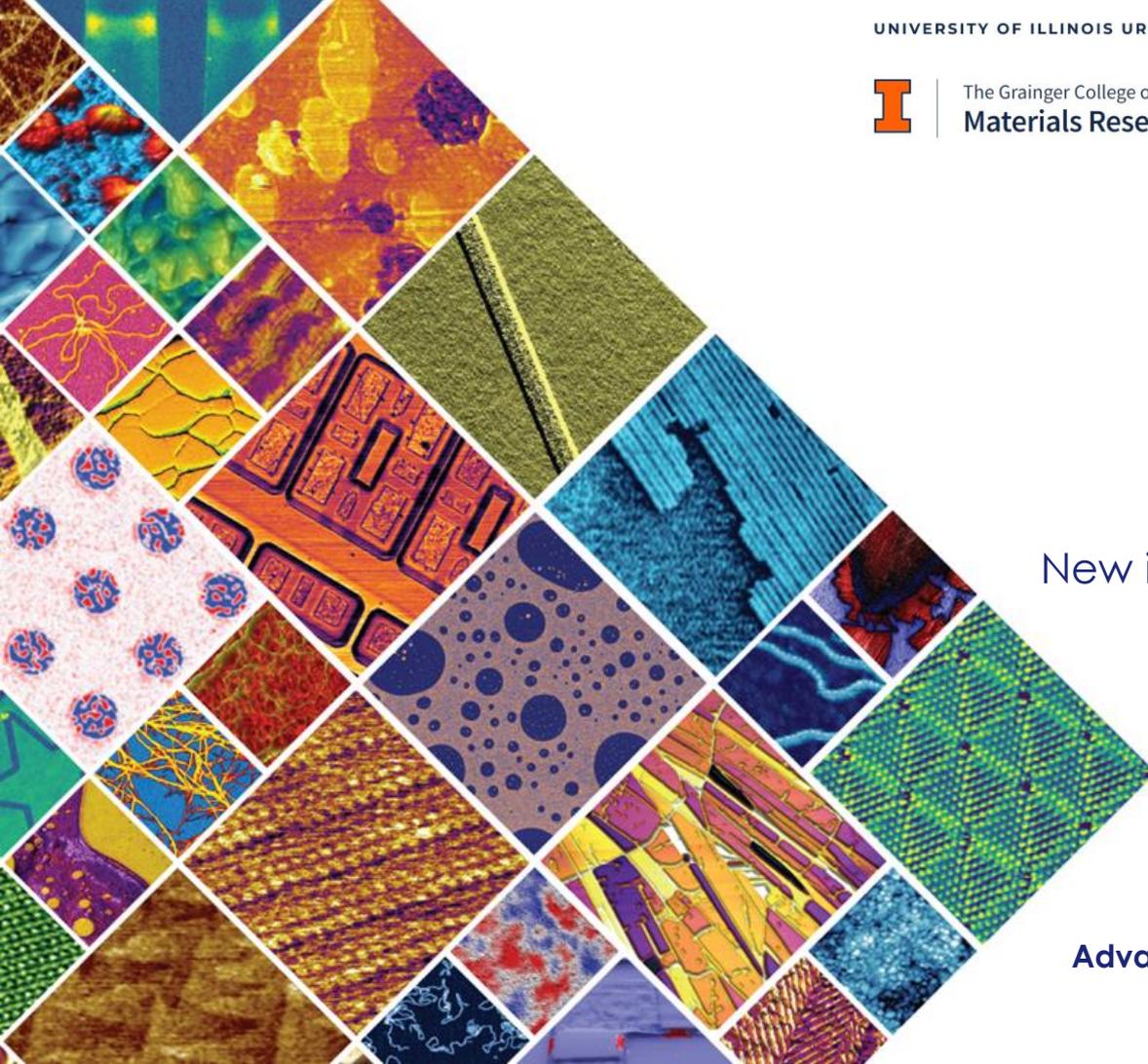
# Can AFMs be more accurate and precise?

New interferometric detection system  
for tip displacement sensing

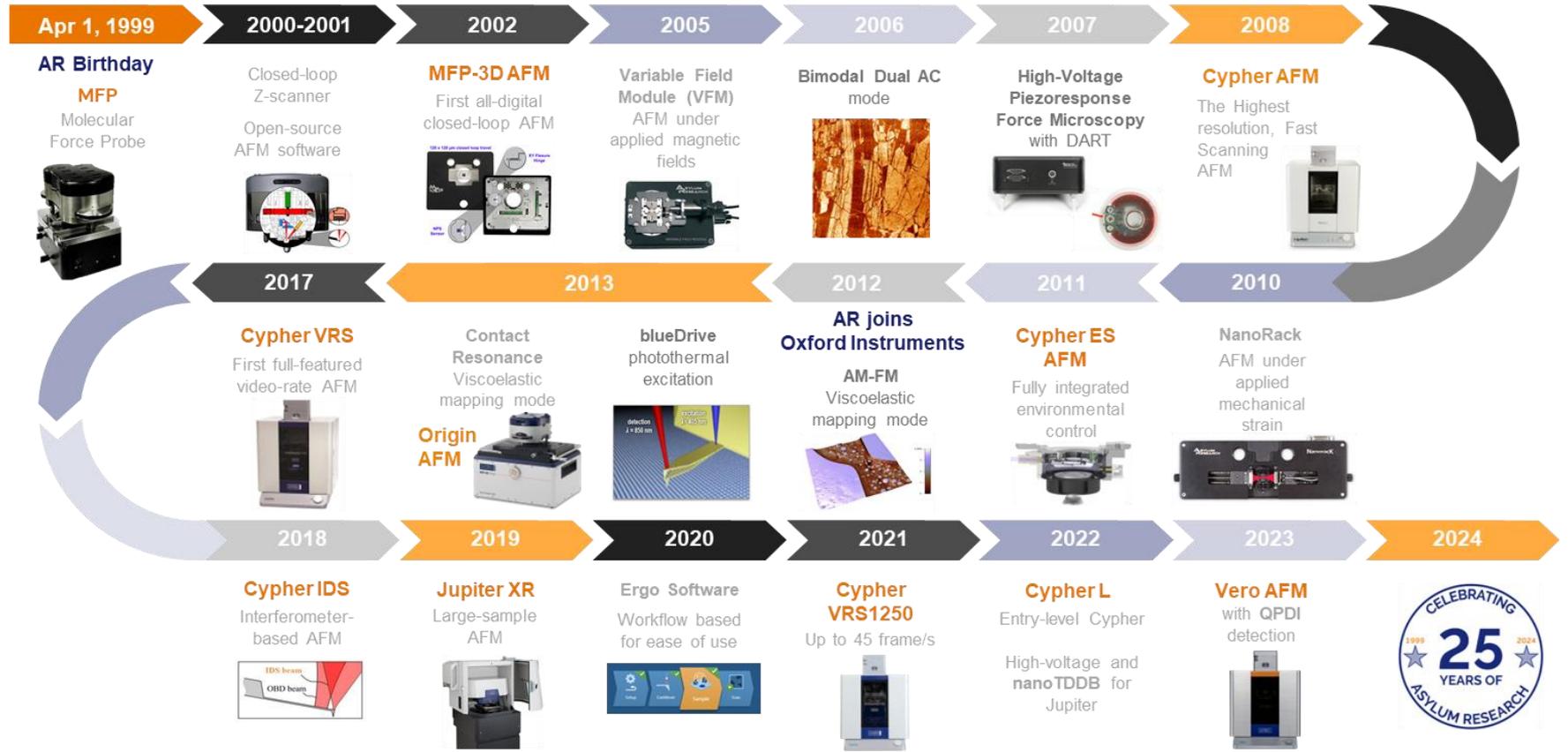
**Ted Limpoco, PhD**

B. Ohler, J. Li, R. Proksch, A. Labuda, J. Lefever  
Oxford Instruments Asylum Research  
Concord, MA ◦ June 2024

**Advanced Materials Characterization Workshop  
University of Illinois, Urbana-Champaign**



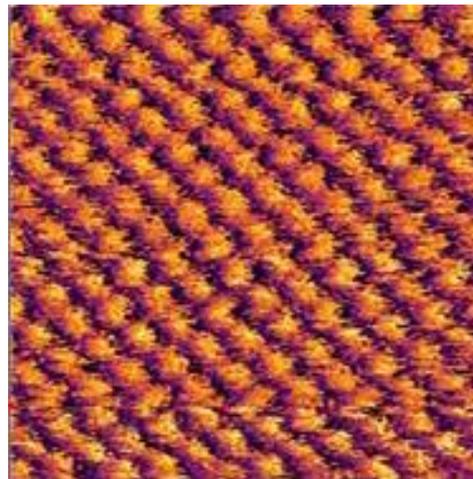
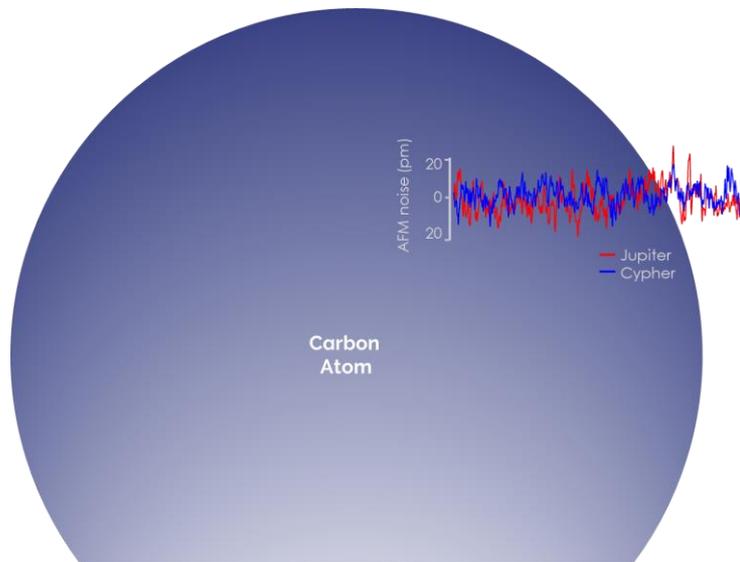
# Innovation through **NEW** products



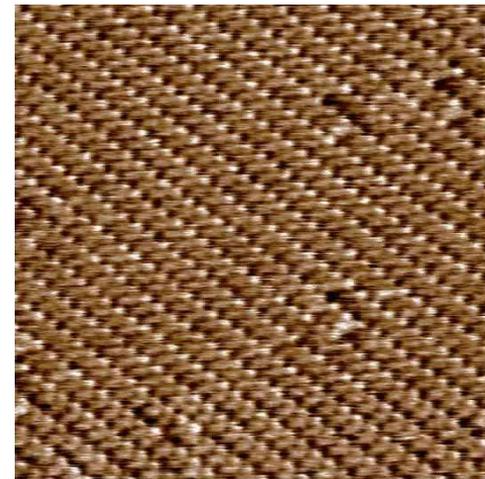
# AFMs = high resolution visualization

## AFMs visualize surface topography... down to atoms

- Sharp stylus (vs. light, electrons)
- Vertical resolution (z-noise <15 pm)
- Lateral resolution (tip radius <10 nm)

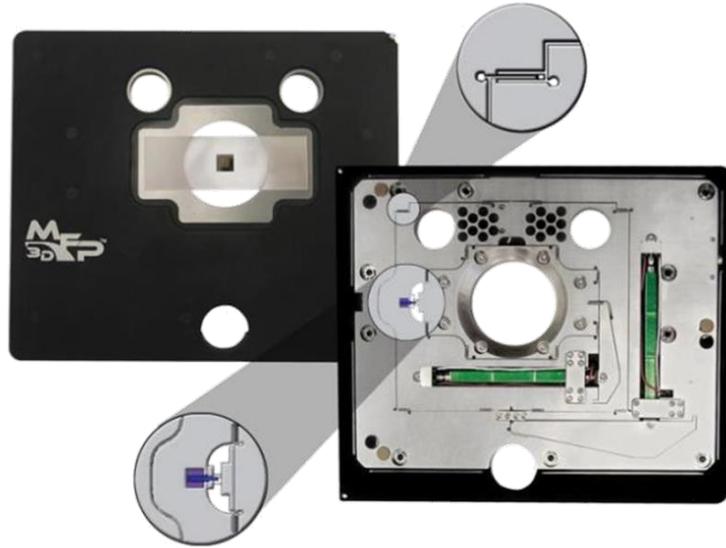


**Graphite lattice**  
1-5 nm scan  
(contact mode - current image)

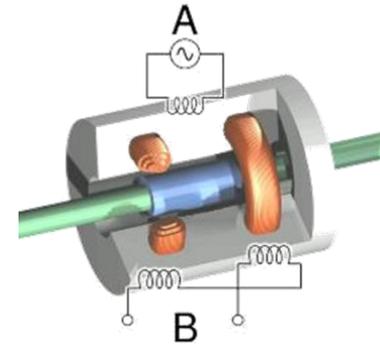


**Calcite point defects**  
10 nm scan  
(tapping mode in liquid)

# AFM = high resolution visualization



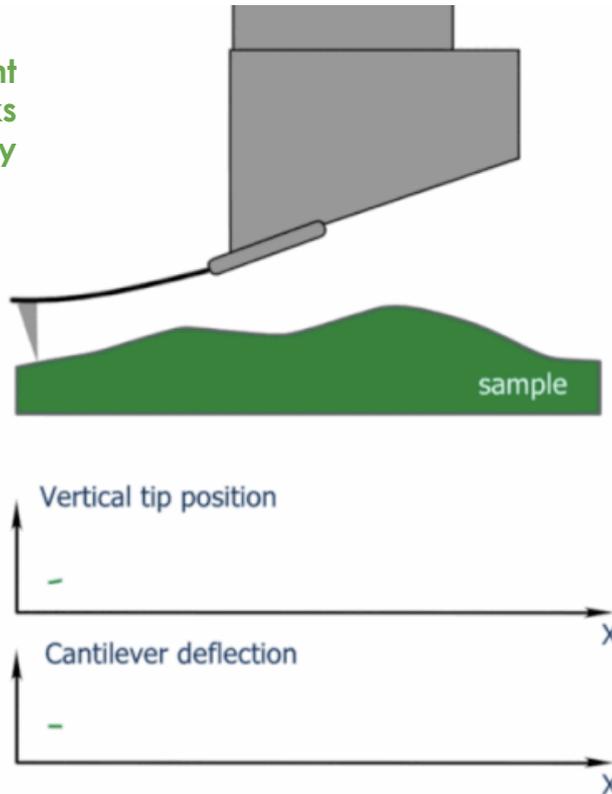
Asylum Research pioneered **closed-loop scanners**, which revolutionized scan accuracy



Asylum Research also developed the **lowest noise position sensors**, improving AFM scanner position

# How is topography obtained?

Z-piezo displacement  
(voltage) tracks  
topography



- In contact mode, the **height feedback loop** looks at deflection
- When an AFM tip is rastered across the surface, cantilever **deflection** changes when the tip encounters variations in topographic slope.
- The height feedback loop **adjusts the tip z-position** to keep deflection at setpoint, i.e., to maintain a constant loading **force**
- The actuating **voltage** to adjust (extend/retract) the z-piezo therefore tracks topography.

# How is deflection detected?

Google atomic force microscope schematic

All Images Videos Forums Flights More Tools

Metamorphic Igneous Biotite Geology Garnet Tholeiitic Basalt Ternary Plot

1. National Institute of Standards and Technology: Schematic of an Atomic Force Microscope

2. Wikipedia: Atomic force microscopy ...

3. ResearchGate: A schematic diagram...

4. NanoAndMore: Atomic Force Micro...

5. ResearchGate: Schematic of an atomic force microscop...

6. Microbe Notes: Atomic Force Microscope: Principle ...

7. ResearchGate: Schematic drawing of the atomi...

8. Wikipedia: File:Atomic force microsc...

9. AZoOptics: Atomic Force Microscopy: Gen...

10. Mechatronics Resea...: Atomic Force Micro...

11. Chemistry LibreTexts: 9.2: Atomic Force Microscop...

12. ResearchGate: atomic force microscopy operation ...

13. LNF Wiki: Atomic force microscopy - LNF Wiki

14. Tribonet: Atomic force microscopy - About Tribology

15. Edinformatics: Atomic Force Microscope

16. Asylum Research - Oxford Instruments: Atomic Force Microscopy - An Overview ...

17. ResearchGate: atomic force microscope (AFM) ...

18. Science Info: Atomic Force Microscopy ...

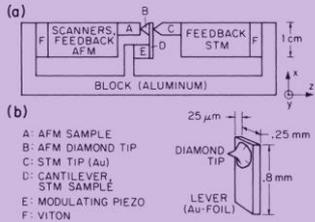
19. AZoNano: TappingMode Atomic Force Microscopy

20. Nanoscience Instruments: Atomic Force Microscopy | Nanos...



# How did we get OBD?

## 1986 AFM Invented

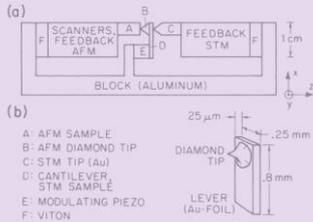


Binnig, G., Quate, C. F. & Gerber, Ch. Phys Rev Lett 56, 930-933 (1986)

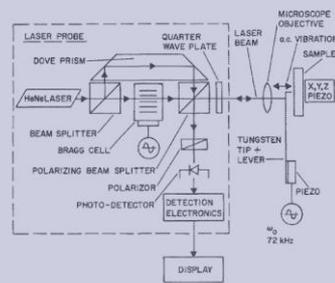
Binnig, Quate, and Gerber's first AFM used an STM!

# How did we get OBD?

## 1986 AFM Invented



## 1987 Interferometric AFM

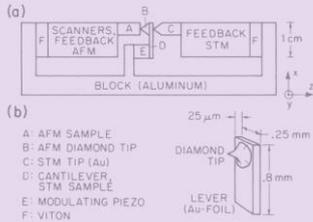


Martin, Y., Williams, C. C. &  
Wickramasinghe, H. K. J. Appl.  
Phys. 61 4723 (1987)

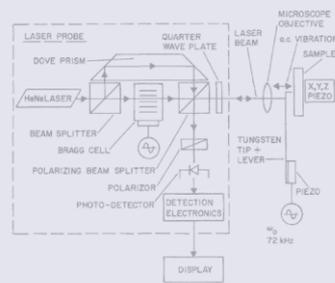
Several early AFM designs used interferometric sensing

# How did we get OBD?

## 1986 AFM Invented



## 1987 Interferometric AFM



## 1988 Optical Beam Deflection "OBD"

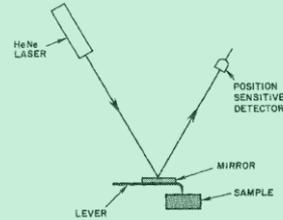


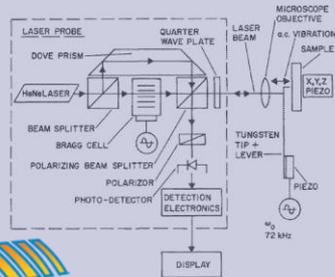
FIG. 1. Cantilever deflection detection scheme.

Meyer, G. & Amer, N. M. Appl Phys Lett 53, 1045-1047 (1988)

Why did OBD become the default?

# Early interferometric AFMs had issues...

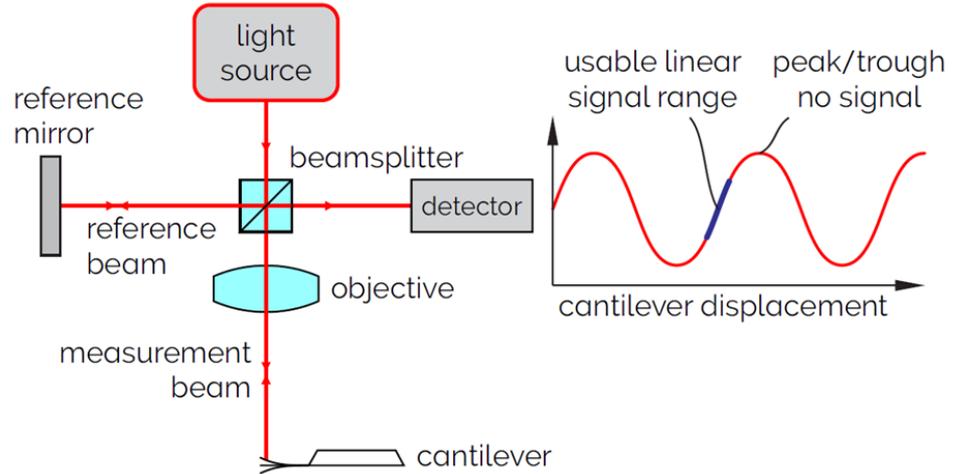
## 1987 Interferometric AFM



**BACK  
TO  
THE  
FUTURE**



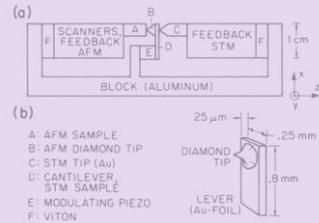
We can't get to  
88 mph for time  
displacement!!!



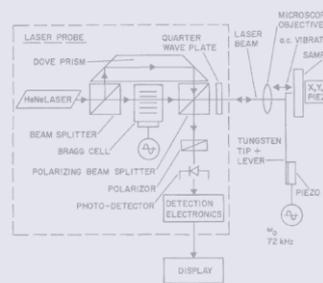
- Limited measurement range
- Poor low-frequency noise / drift
- Complex to build and use

# Revisiting interferometric detection

## 1986 AFM Invented



## 1987 Interferometric AFM



## 1988 Optical Beam Deflection "OBD"

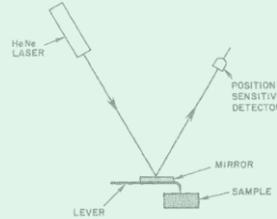
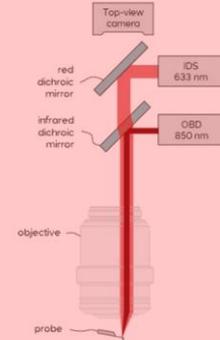


FIG. 1. Cantilever deflection detection scheme.

## 2018 Cypher IDS



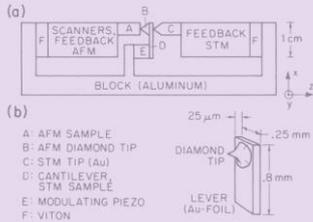
Labuda, A., & Proksch, R.  
Appl. Phys. Lett. 106  
(2015)

30 years  
later...

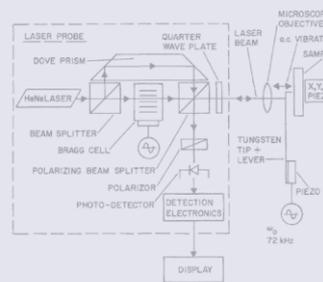
**Cypher IDS:** interferometric detector demonstrating benefits for piezoresponse force microscopy (PFM). But still poor low-frequency noise...

# New in 2023: AFM with QPDI detector

## 1986 AFM Invented



## 1987 Interferometric AFM



## 1988 Optical Beam Deflection "OBD"

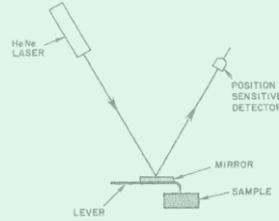
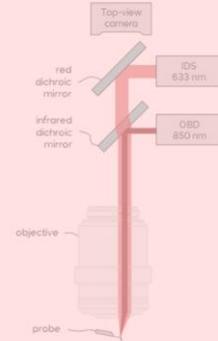
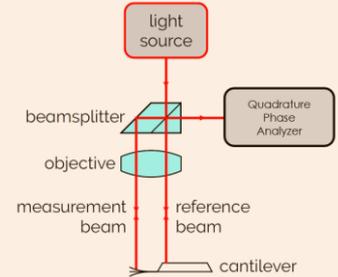


FIG. 1. Cantilever deflection detection scheme.

## 2018 Cypher IDS



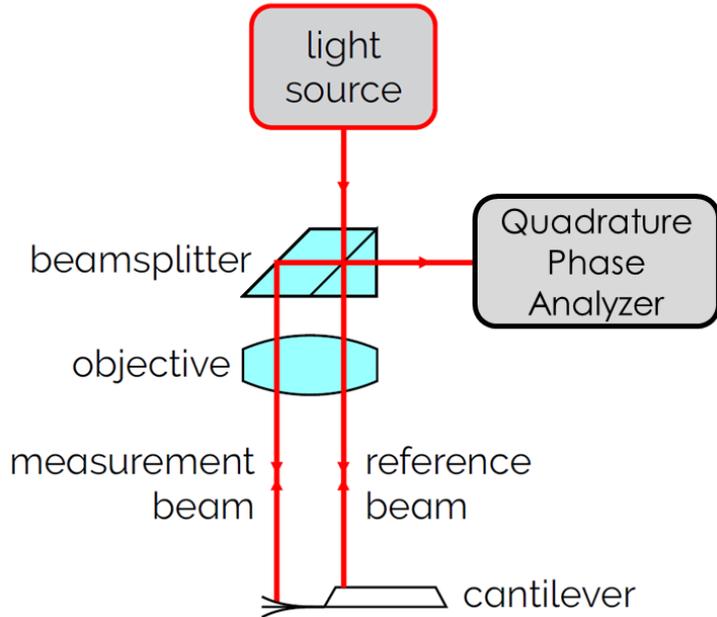
## 2023 Vero



Fall MRS  
2023

**Vero:** first AFM to use quadrature phase differential interferometry (QPDI) detector.

👉 So what is different about QPDI? 👉



**“Quadrature Phase”** Two interferometric signals are generated, where the second has a  $90^\circ$  phase delay with respect to the first... a bit like running two interferometers in parallel

👍 Benefit: QPDI can measure very large displacements and do so while maintaining optimal noise performance

**“Differential”** Instead of using a remote reference mirror, the back of the probe substrate acts as the reference, i.e.,  $<1$  mm from the AFM tip

👍 Benefit: QPDI has dramatically better low-frequency noise and drift

# Vero: very accurate and very precise

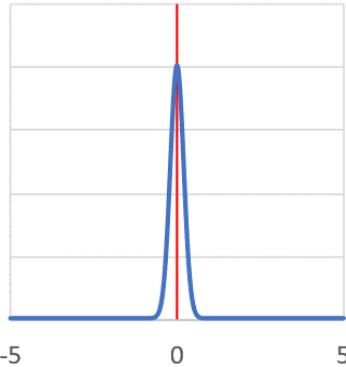
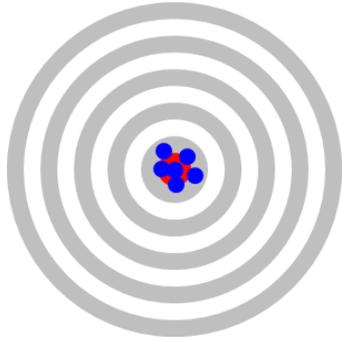
Vero nihil  
verius!



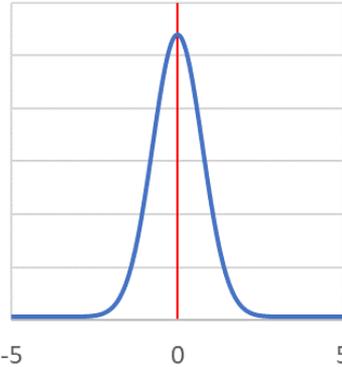
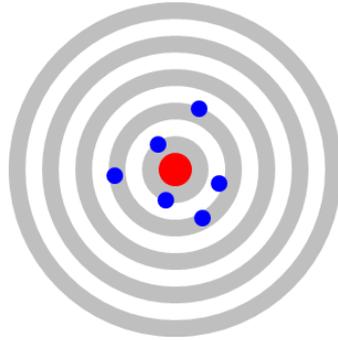
- Vero is a next-generation AFM family from Oxford Instruments Asylum Research
- Vero uses **Quadrature Phase Differential Interferometry (QPDI)** to produce more accurate and precise AFM results
- Vero builds on the ultra-high performance, stability, and capabilities of Cypher AFMs

# Accuracy and precision

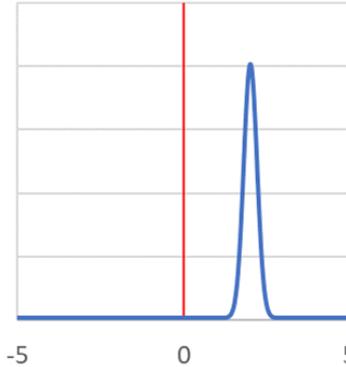
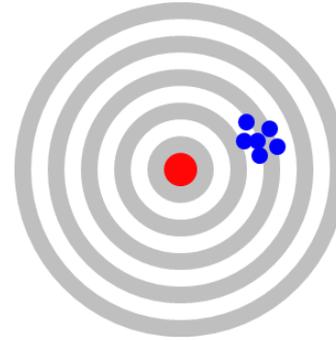
Accurate  
and precise



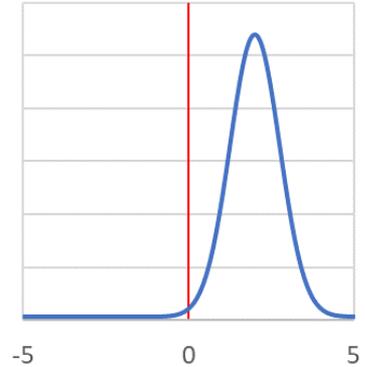
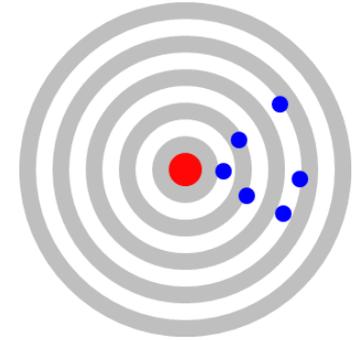
Accurate  
but less precise



Less accurate  
but precise



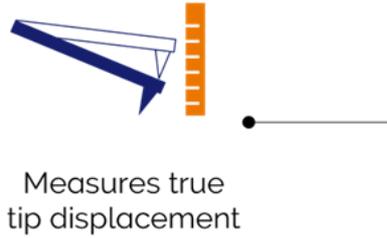
Less accurate  
and less precise



# Five key benefits



# Five key benefits



Avoids crosstalk between vertical and in-plane tip forces



Improves measurement sensitivity with lower noise detection



More accurate and repeatable results



Is precisely calibrated by the wavelength of light

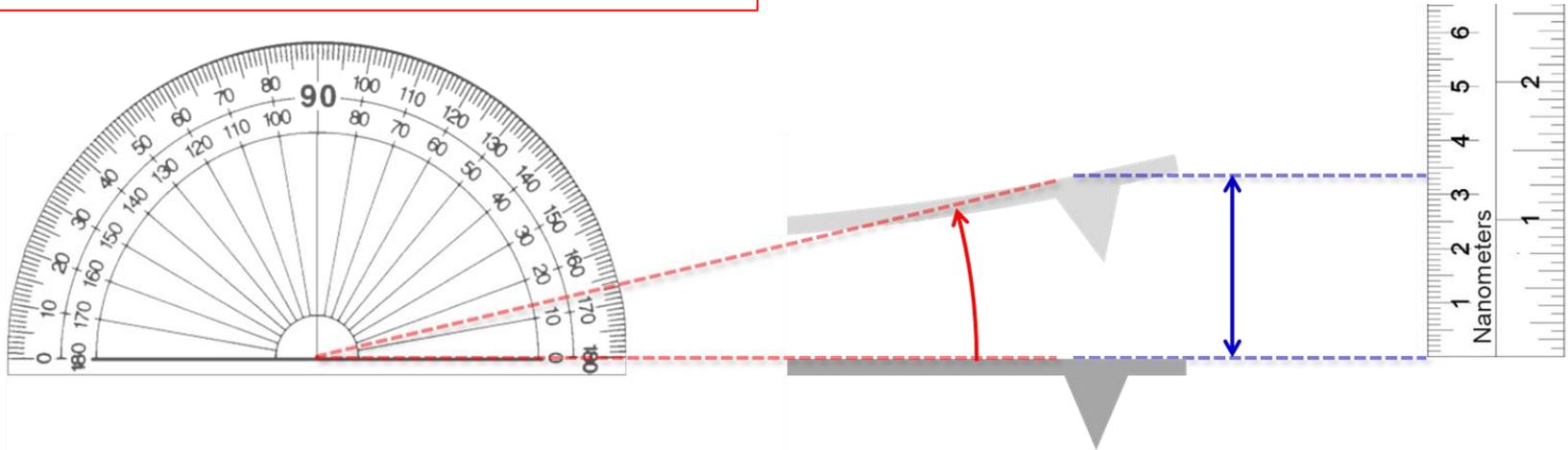
# Vero measures true tip displacement

## Optical beam deflection (OBD)

- OBD measures **cantilever angular changes**
- Angular changes must be converted into displacement
- Conversion value (optical lever sensitivity or "InvOLS") is dependent on many factors (e.g., spot position, spot size, cantilever length, etc.)

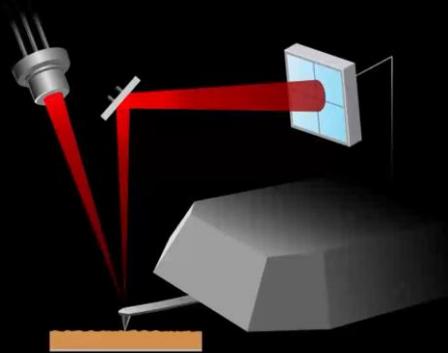
## Quadrature phase differential interferometry (QPDI)

- Vero QPDI measures **tip displacement** directly
- "InvOLS" is a fixed constant (510 nm/V)



# You can't solve OBD errors with better calibration

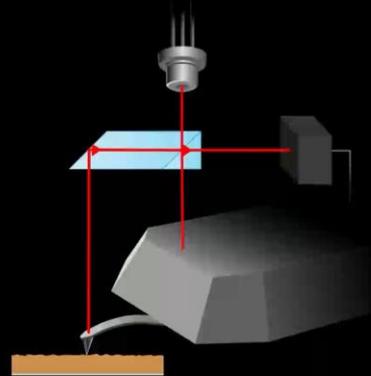
## OBD measures angular deflection



OBD Cantilever Deflection



## QPDI measures tip displacement



QPDI Tip Displacement



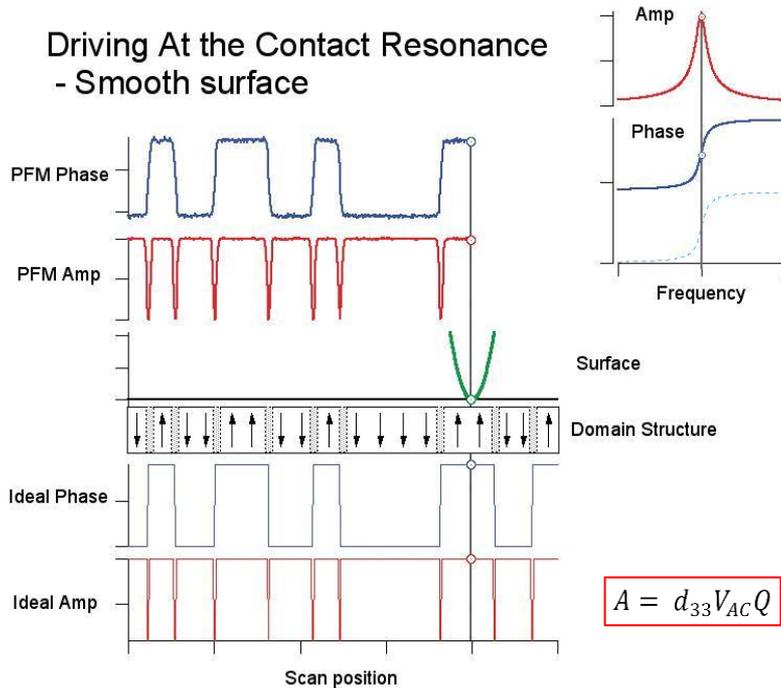
- All angular changes are interpreted as tip displacement
- But lots of things can affect cantilever bending besides tip displacement

- No tip displacement detected even when there is cantilever bending

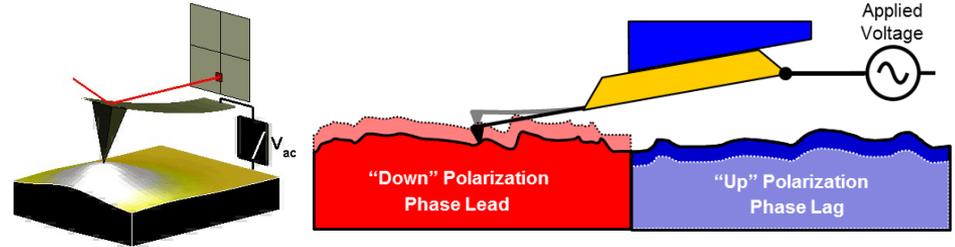
**When does this happen?**

# Piezoresponse force microscopy

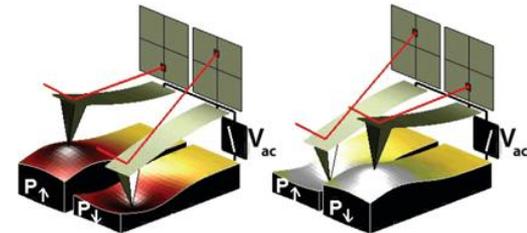
## Driving At the Contact Resonance - Smooth surface

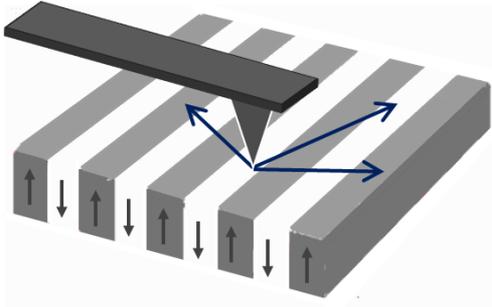


$$A = d_{33} V_{AC} Q$$



- **Amplitude** is related to the magnitude of the bias and the "effective" vertical piezo coefficient, ( $d_{\text{eff}}$ )  
PFM  $d_{\text{eff}}$  values range from 0.1 pm/V to 500 pm/V
- **Phase** gives directional information, i.e., domain polarization:



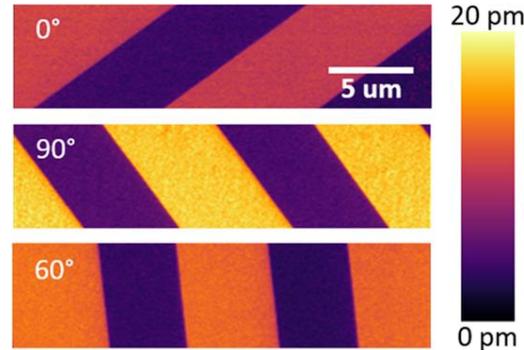


## PFM imaging on PPLN

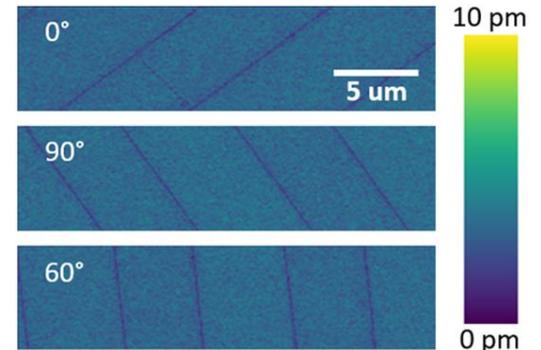
### Periodically poled lithium niobate (PPLN)

- Patterned with up and down domains
- Same material but oppositely polarized
- Magnitude of piezoresponse should be the same

#### OBD (inaccurate)

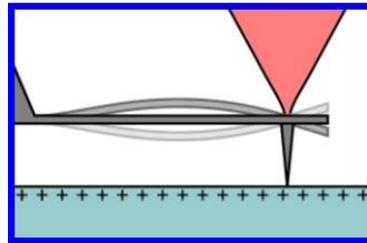
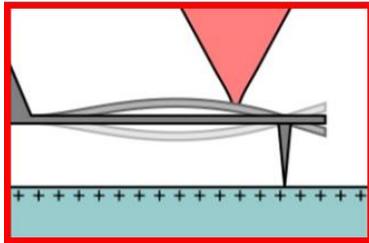


#### Vero QPDI (accurate)

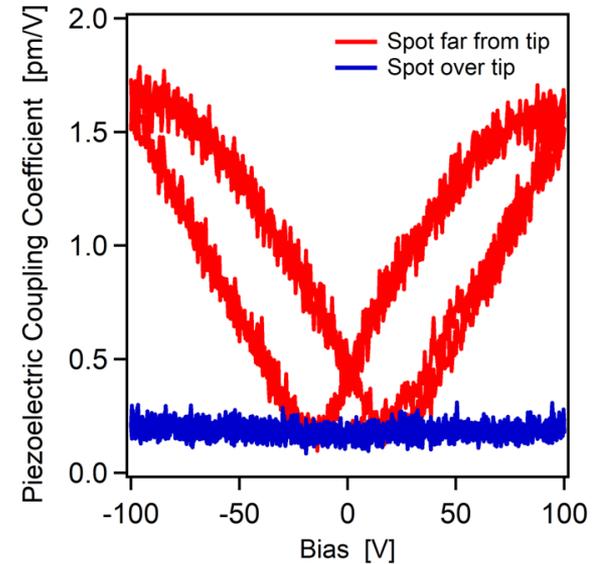


- **Tip-sample friction** contributes to cantilever bending
  - OBD shows inaccurate **variation in amplitude** of piezoresponse, as well as **variation with scan angle**
  - Due to variable in-plane forces from friction
- QPDI detection not affected by tip-sample friction

- During PFM, drive bias can drive the cantilever via **electrostatic forces**
- Soda lime glass, though not ferroelectric, can exhibit cantilever oscillation if...
  - OBD is used (measures cantilever angle)
  - QPDI is used if spot isn't over the tip
- PFM with QPDI unaffected if spot is over tip



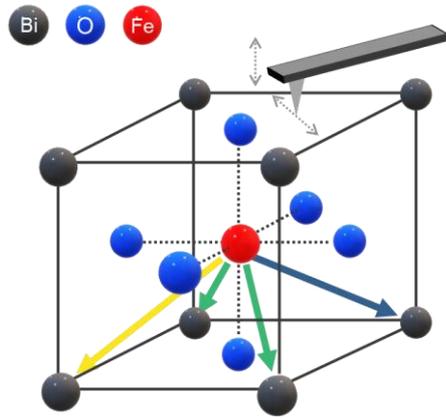
## QPDI SS-PFM on soda lime glass



**X** inaccurate  
**✓** accurate

# Five key benefits

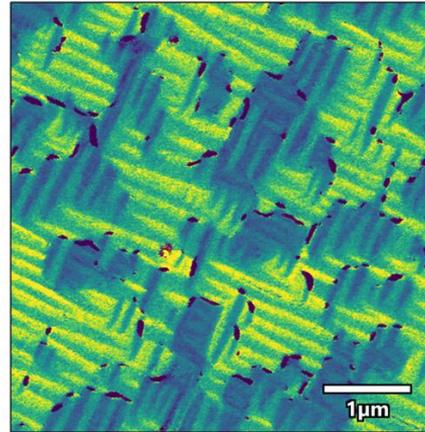




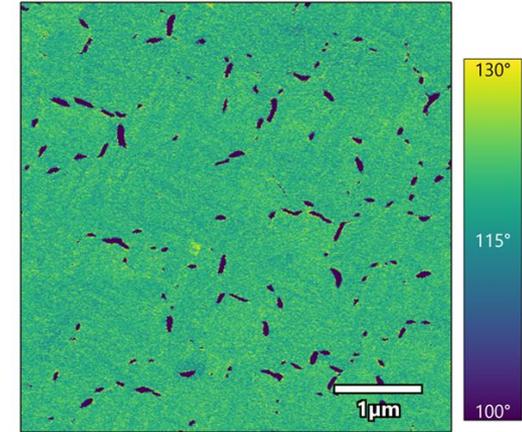
- Many piezoelectric materials exhibit both in-plane and out-of-plane response
- PFM response on BFO (100) has both in-plane and out-of-plane response

## PFM on bismuth ferrite ( $\text{BiFeO}_3$ or “BFO”)

**OBD** (inaccurate)



**Vero QPDI** (accurate)

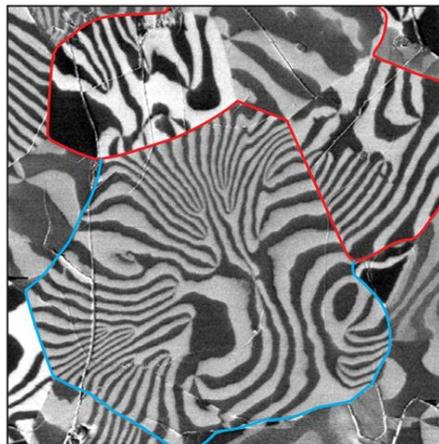


- **Crosstalk** of in-plane response into vertical response
  - OBD-based PFM claims to distinguish between vertical and lateral response, but in-plane tip-sample forces couple into the vertical deflection
- QPDI vertical response unaffected by in-plane forces

## PFM on erbium manganese trioxide ( $\text{ErMnO}_3$ )

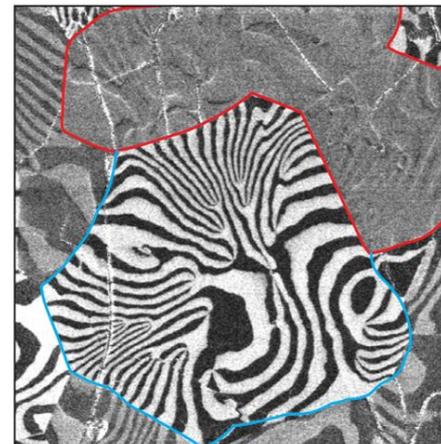
- **Crosstalk** of in-plane response into vertical response
  - **Red outline** highlights grains that have mostly in-plane response.
  - **Blue outline** highlights grain with out-of-plane response.
  - In plane response is visible in OBD (artifact) but not in QPDI.
- Note: DART used in OBD to accentuate signal

**OBD** (inaccurate)



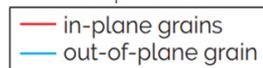
$(f_{\text{DART}} \sim 350 \text{ kHz})$

**Vero QPDI** (accurate)

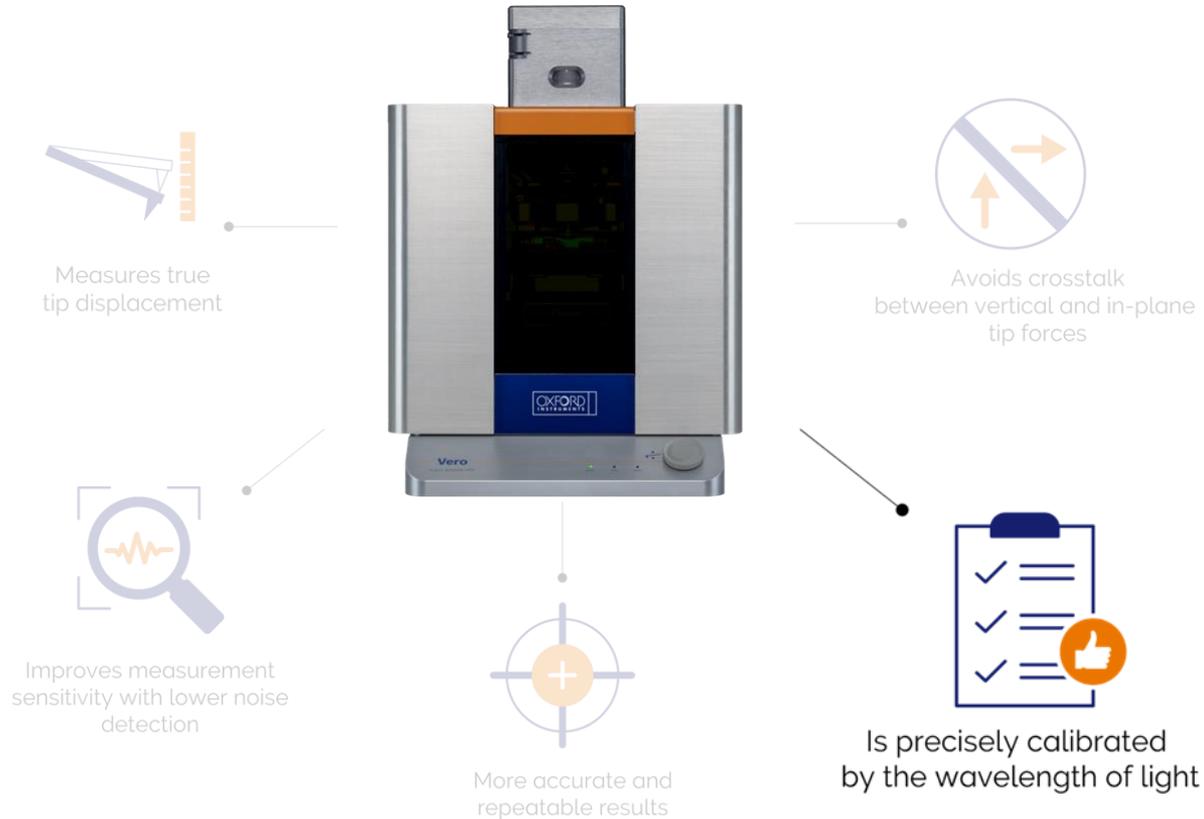


$(f_{\text{drive}} \sim 30 \text{ kHz})$

15  $\mu\text{m}$  scan



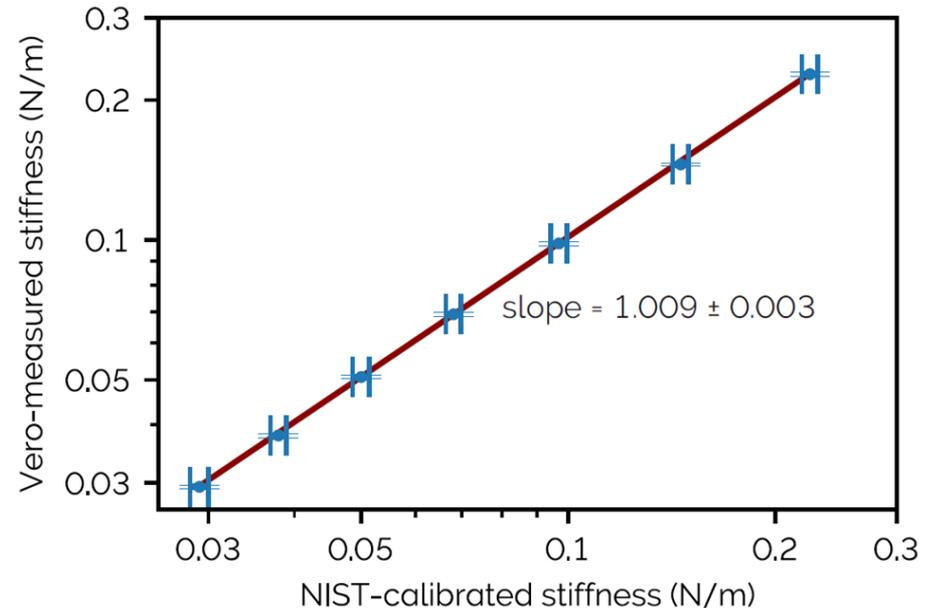
# Five key benefits



# Accurately calibrates spring constants

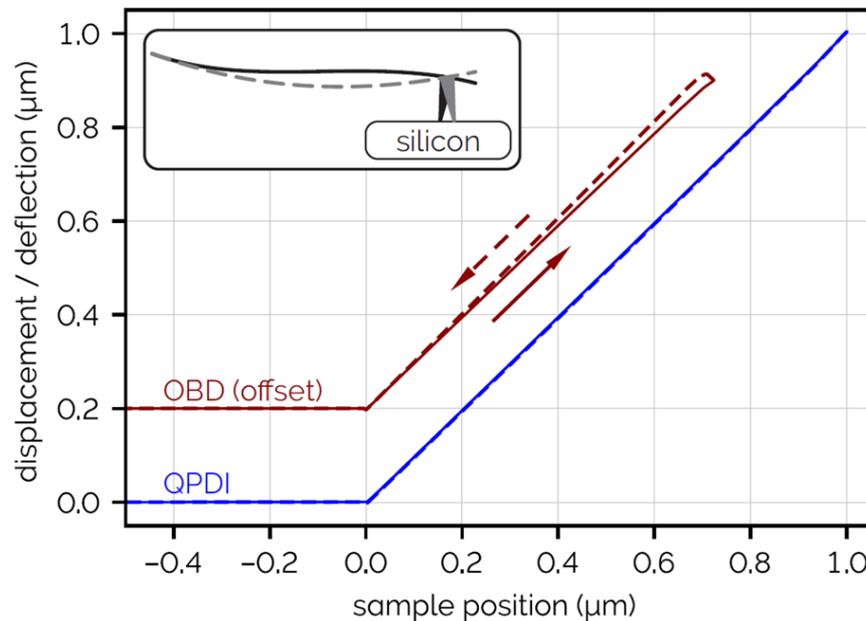
- With OBD, **10-20% error** in cantilever spring constant calibration is typical.
- Vero's built-in interferometer and direct measure of tip displacement reduces this error.
- Sensitivity (InvOLS) is fixed by the wavelength of light used (510 nm/V)

Vero QPDI spring constant calibrations agreed with NIST SI-traceable values **to within 1%**



# Accurately removes buckling in force curves

- Force curve on a hard surface:
  - Extend and retract curves should be linear and overlap if there's no indentation
  - Tip slides and pivots during contact
- Tip-sample friction can cause **buckling** that results in cantilever angular change
  - OBD interprets this as tip displacement, resulting in hysteresis at the turnaround
  - Pivoting of the tip does not change its vertical displacement, so QPDI signal is not affected
  - Tip “plowing” is real and probably affects indentation, but it shouldn't appear in the force curve



# Five key benefits



Measures true  
tip displacement



Avoids crosstalk  
between vertical and in-plane  
tip forces



Improves measurement  
sensitivity with lower noise  
detection



More accurate and  
repeatable results



Is precisely calibrated  
by the wavelength of light

# Detector with the lowest noise floor

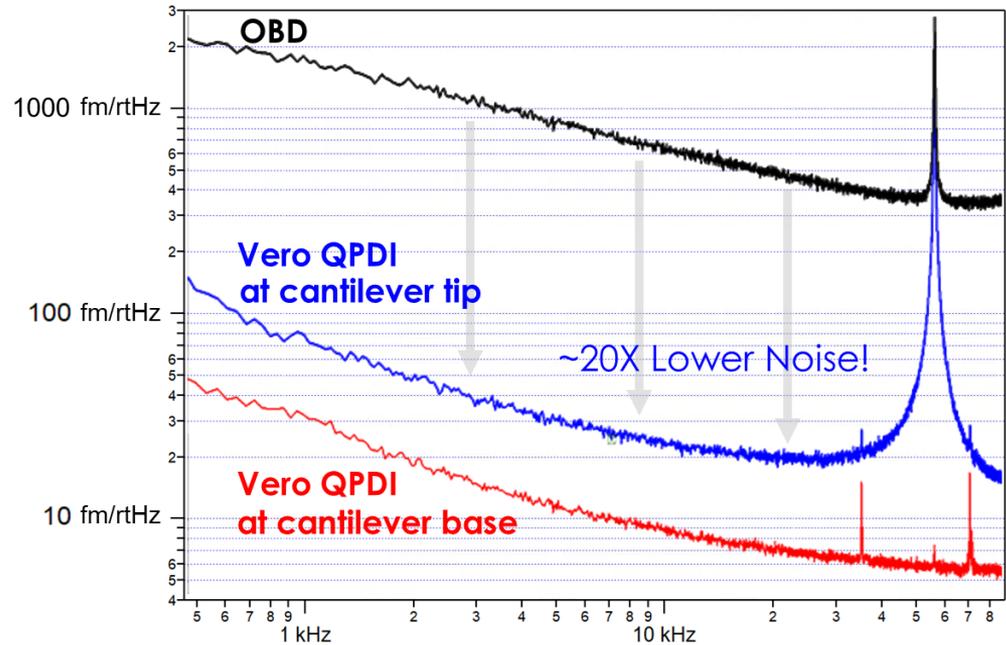
## OBD

- Noise floor depends on cantilever size vs. spot size
- Best case:  $\sim 25 \text{ fm}/\sqrt{\text{Hz}}$  if carefully optimized, but usually  $200\text{-}500 \text{ fm}/\sqrt{\text{Hz}}$

## QPDI

- Noise floor does not depend on cantilever size vs. spot size
- Consistently  $< 10\text{-}20 \text{ fm}/\text{rtHz}$  above  $20 \text{ kHz}$  regardless of cantilever or spot size
- Actual **detector noise** can be measured at the base
- So signal at the tip is actual **sub-resonance thermal motion**
- This means what we are seeing is thermally limited motion even for stiffest levers

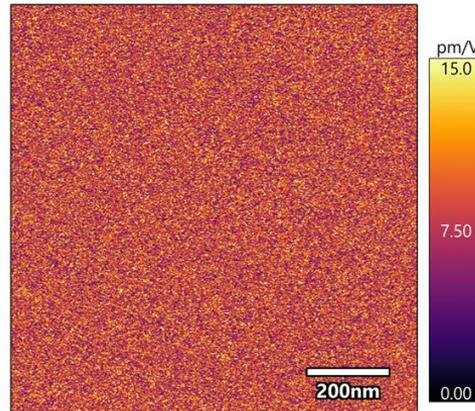
**Adama AD-2.8-AS probe**  
( $w \sim 35 \mu\text{m}$ ,  $l \sim 225 \mu\text{m}$ ,  $f \sim 65 \text{ kHz}$ ,  $k \sim 2.8 \text{ N/m}$ )



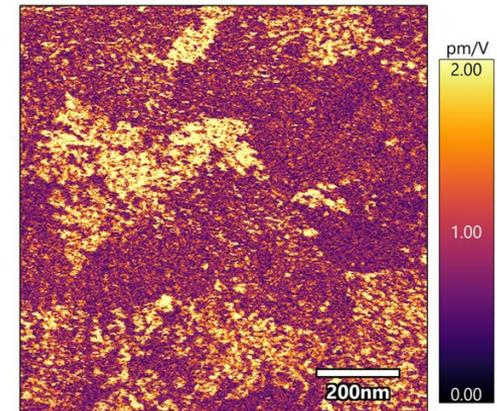
- $\text{HfO}_2$  is uniquely compatible with Si and can be naturally **integrated in logic and memory devices**
- Processing into thin films is key to transforming  $\text{HfO}_2$  into its ferroelectric crystalline state
- Vero clearly **resolves piezoelectric domains** in hafnia even though the response is  $< 2 \text{ pm/V}$
- Identical settings used for these two images. Only difference is detector type (OBD vs QPDI)
- DART or HV - but will not work on samples with low breakdown or coercive voltage

## PFM on hafnia ( $\text{HfO}_2$ )

OBD (weak signal)



Vero QPDI (strong signal)

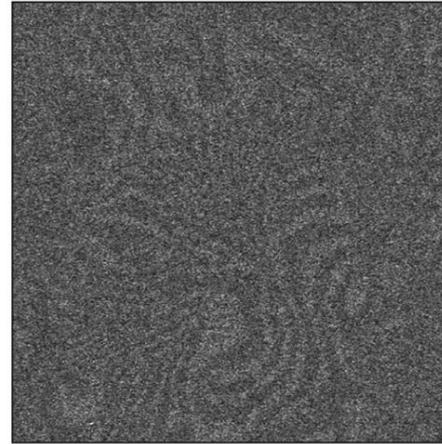


Technique: single-frequency PFM at 30 kHz, 2 V drive amplitude, and 290 nN setpoint

## PFM on erbium manganese trioxide ( $\text{ErMnO}_3$ )

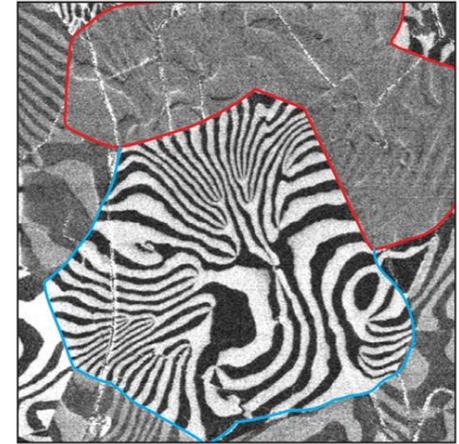
- Identical settings used for these two images. Only difference is detector type (OBD vs QPDI)
- Vero clearly **resolves piezoelectric domains** which highlights much lower noise floor of the QPDI detector
- DART (resonance amplification) an option, but may still contain artifacts

OBD (weak signal)



$f_{\text{DART}} \sim 350 \text{ kHz}$

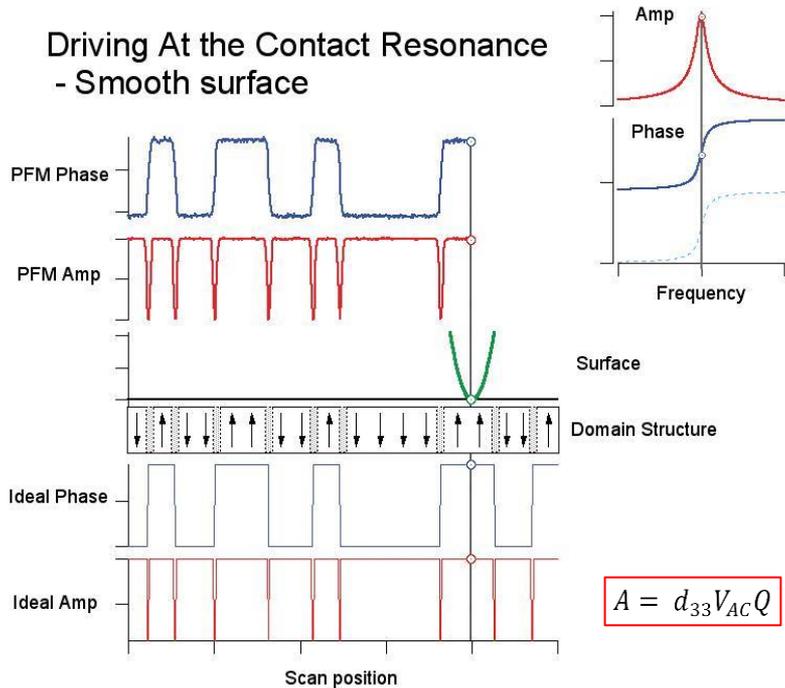
Vero QPDI (strong signal)



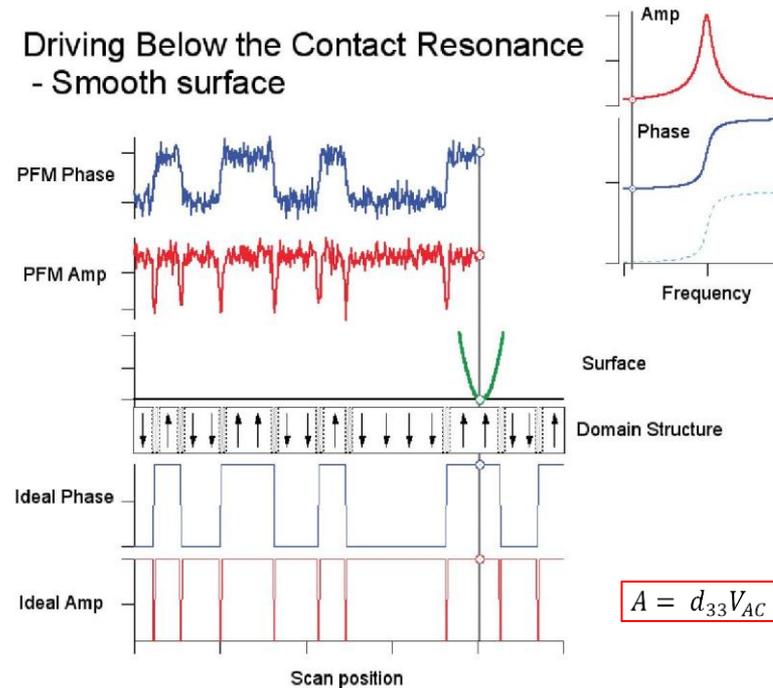
$f_{\text{drive}} \sim 30 \text{ kHz}$

# On-resonance vs. Off-resonance PFM

## Driving At the Contact Resonance - Smooth surface

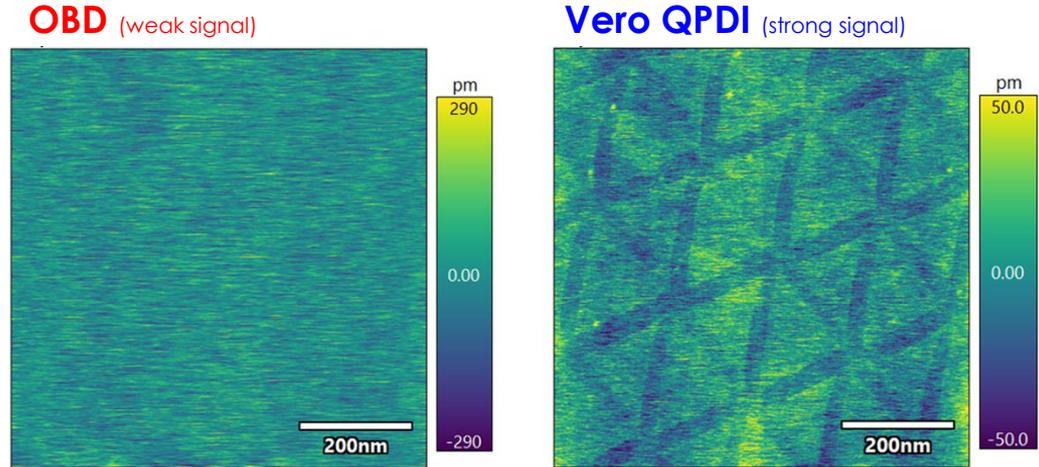


## Driving Below the Contact Resonance - Smooth surface

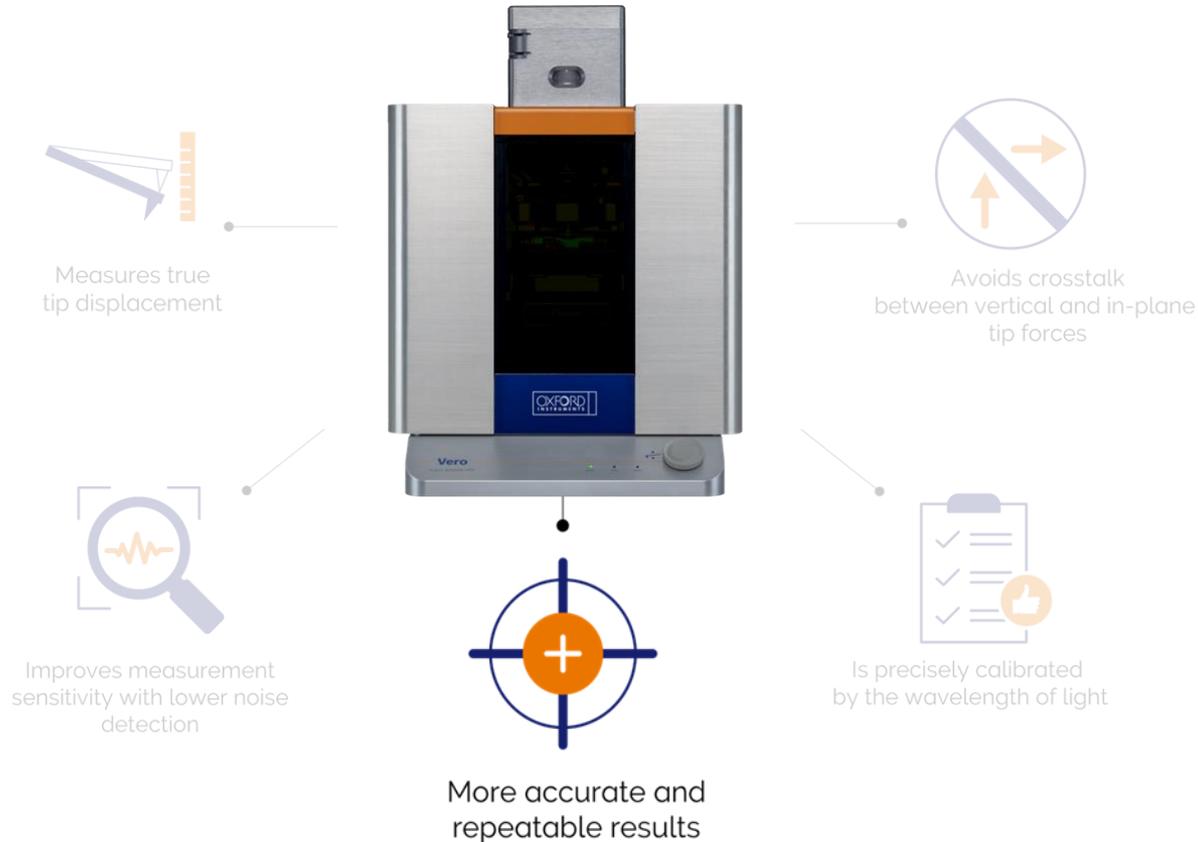


- **Moiré patterns** form when 2D materials are stacked
- Varying the relative rotation (or **twist angle**) alter their electronic properties
- tBLGs can either be superconductors or correlated insulators within a narrow range of “magic” angles around 1.1 degrees.
- Moiré pattern typically not observed in **topography** so other contrast mechanisms used (LFM, PFM)
- Owes to the **low noise floor** of Vero
- What else can Vero potentially see?

## Twisted bilayer graphene (tBLG) moiré

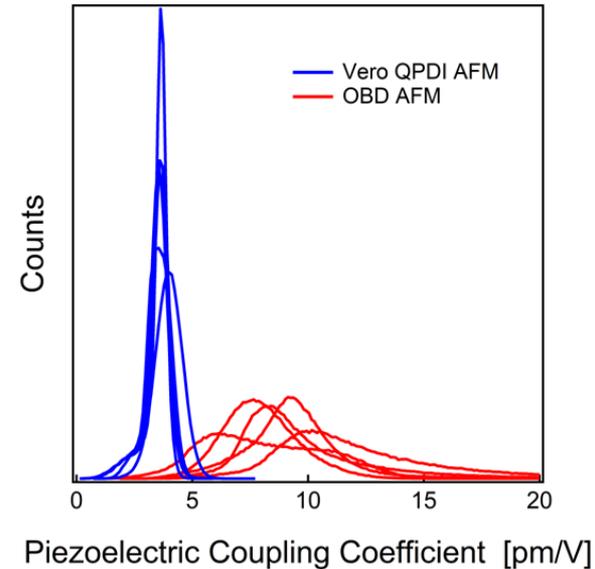


# Five key benefits



- AlN (a piezoelectric material) is used in **acoustic resonators** in wireless devices
- Many advantages, e.g., compatible with high temperature, CMOS processing, etc.
- But has low piezoresponse (6 pm/V)
- Alloying AlN with Sc increases response by up to 4x
- **Processing needs to be optimized**, e.g., balanced with defects at higher Sc concentrations
- Requires **good correlation with Sc levels and piezoresponse** to evaluate processing
- Vero QPDI results show both more precise measurements (narrower distributions) and more repeatable measurements (peaks tightly clustered) compared to OBD

## PFM of scandium aluminum nitride (ScAlN)



Technique: single-frequency PFM at 30 kHz, 1-5 V drive amplitude, and 290 nN setpoint

## Accuracy (systematic errors)

- Measurement artifacts
  - Electrostatic artifacts in PFM measurements
  - Pivoting or buckling of tip during force curves
- Calibration errors
  - Error in INVOLS calibration (aka deflection sensitivity)
  - Error in spring constant calibration



## Precision (random errors)

- Measurement noise
  - Noise in OBD deflection signal
  - Dependence of noise on cantilever
- Calibration repeatability
  - User variability in INVOLS calibration
  - User variability in spring constant calibration



# Thank You! Questions???

## Vero AFM Redefined

